possible solutions may be appropriate. The system of dehumidification chosen is the best one for maintaining and preserving the ship, but it will nonetheless require careful application and close monitoring.

34. Recommendation 5 Conservation treatment of the hull

- 34.1. The vessel's topsides should remain exposed to the environment, above the glass plane, in order to present the vessel in a manner that greatly aids visitor comprehension and quality interpretation.
- 34.2. The dome headed bolts on the hull exterior should be removed and the resultant holes filled with GRP and finished flush with the surface of the plates. This would have the advantages of removing material that could cause galvanic corrosion and make the ship more closely resemble her pre-timber-clad days. Liaison with a conservation engineer would be required to ensure that the structural stability of the ship was not compromised by this change.
- 34.3. The topsides will need to be thoroughly cleaned to SA2 or SA 2 1/2, and any areas of failing GRP removed. This treatment should continue to a level just below the level of the glass plane.
- 34.4. Any replacement GRP patches should cover the minimum amount of iron, commensurate with providing an adequate seal and adhering properly. They should be fitted only after the iron has been adequately cleaned and conserved. Large patches will be reinforced. The colour and texture of the patches will be determined in conjunction with the curator, to reflect the interpretative requirements. Where holes are large enough to span frames, it may be prudent to replace GRP with textured steel, if it is possible to achieve this without the loss of original iron.
- 34.5. The hull both above and below the waterline will need to be cleaned, and areas of loose scale will need consolidation. It is not possible to specify exactly what form of cleaning will be required on each part of the ship. This decision will be taken by the conservator and the curator on an area-by-area basis, as the cleaning takes place.
- 34.6. Appropriate paint coatings will need to be applied, once the surface is as clean as possible. The paint coatings will need to be sympathetic to the curator's interpretation of the ship's original colour scheme.

35. Recommendation 6 Drainage and moisture control

- 35.1. The system of drainage pipes installed within the ship in the 1970s needs to be re-designed to mesh with the drainage channel and inlet drains on the steel weather deck.
- 35.2. The original lead scuppers should be reconnected to the hull to allow full functionality.

- 35.3. Water draining from the ship to the dry-dock floor should flow through flexible pipes to avoid splash-back
- 35.4. The outlets from the hull should be reduced to a minimum (preferably one) and piped directly to the dock waste water disposal system.
- 35.5. On rainy days, a considerable amount of moisture can be brought onto the ship by visitors. Cloakrooms should be provided and people encouraged to use them.

36. Recommendation 7 Improvements to services

- 36.1. Given the risk of fire and explosion, the general use of gas and heat on the ship should be strictly controlled and avoided where possible. Where there is no alternative, formal risk assessment should be undertaken and hot works permits issued. The permit should include a requirement to finish generating heat at least four hours before ceasing work and that all gas equipment be removed from the ship and its environs at the end of each working period. Gas sensors should be fitted within the ship.
- 36.2. The galley should be sited on the dockside if the caterers cannot manage without gas-fired equipment. This would confer other advantages as well as reducing the risk of explosion and fire such as reduction in water vapour in the ship. It would also make it easier to allow for a larger space to be left between the galley panelling and the hull. If the galley cannot be re-sited, it should be made all electric. This would also reduce the production of water vapour on the ship, although not by as much as relocating the galley.
- 36.3. The heating system should be removed from the after tank top hold and sited in a new plant room. Hot and/or conditioned air could be ducted into the ship as required. Should dehumidification of the ship be adopted as the conservation method, the equipment necessary for this task should as far as is possible be located off the ship. The irregular offset to the port side of the dry dock might provide an appropriate place for such equipment. In practice, however, the dehumidification task might require separate machines for dealing with the ship and the dry dock. In that case, ducting requirements might make it more appropriate to have the machine located within the ship.
- 36.4. The electrical system of the ship and the surrounding buildings should be rewired to reduce the risk of fire, increase safety and render the system more easily understood. Existing services should be stripped out rather than modified or adapted. New services should be installed appropriate to requirements and modern standards.
- 36.5. The ship should be fitted with a new, purpose designed automatic fire fighting system. This should be permanently active, fully accessible to all members of staff at all times, and not require coupling before use.

- 36.6. As an interim measure, the three-inch fire main currently in use should be permanently attached to a water supply.
- 36.7. In general, the services of the ship should be modernised, rationalised and, where possible, centralised. A new plant room should be created to accommodate main electrical distribution & control equipment, heating equipment, dehumidification equipment, pump controls and fire-fighting controls.

37. Recommendation 8 Structure of the Ship⁸⁰

- 37.1. A compound armature should be built within the ship which relies on keel, bulkheads, stringers and frames to strengthen the ship's pre 1970s iron.
- 37.2. The columnar structure of the ship should be reinforced to transmit loads from deck to tank top. Concentrate these loads on to the keel which will serve as the foundation. Pass the concentrated linear load through the keel blocks to a new beam inserted above the dry dock keel stones to ensure as even a distribution as possible to the existing foundation system. The weight of the new system should be kept to an absolute minimum.
- 37.3. Special concentrations of load, such as those arising from the engine should be catered for by providing individual foundations.
- 37.4. Attachment of the new armature to the existing system is crucial. It should be unobtrusive and be linked as closely as possible to the curatorial requirement to open up as much of the ship as possible for public access and interpretation and to the conservation requirement to treat and seal various parts of the ship.
- 37.5. The attachment method must be minimalist in its interference with the ship's original material. However, there may be areas of the ship where the decision to remove, modify or otherwise interfere with original material has to be taken, for the sake of preservation of the ship as a whole. To this end, when installing the armature, a hierarchy of allowable intervention has been agreed:
 - 37.5.1. Alterations and adaptation of post 1970's construction can be freely made;
 - 37.5.2. Existing holes or fake bolts may be used for attachment;
 - 37.5.3. If no alternative exists, existing rivet holes may be used.

 Where the rivet must be removed, this will be done as sensitively as possible, after full curatorial approval.

 Experimentation will be required to determine a method of rivet removal that will preserve as much of the rivet as possible

⁸⁰ The recommendations for structural support modifications are based largely on suggestions proposed by Julian Harrap Architects

- Other interventions with the potential to damage or remove original material must be considered on a case by case basis to ensure there is no alternative, and would only be countenanced in exceptional circumstances. Any alteration to the ship's fabric should include an appropriate archaeological recording element.
- 37.6. Any modern concrete in the hull that is considered to be harbouring corrosive compounds & moisture holding materials and increasing weight in a manner that is deleterious to the vessel should be removed, unless it is important to the structural stability of the ship. Any removal of concrete should be undertaken in close liaison with a conservation engineer and may require the insertion of additional support steel-work.
- 38. Recommendation 9 The dry-dock
- 38.1. There are three factors which dictate appropriate work on the dry dock:
- 38.2. First, that the conservation needs of the ship must be met by ensuring that the protection afforded to the ship by the dry dock environment is adequate. This will largely consist of measures aimed at improving the drainage into the sumps and ensuring a higher standard of water-tight integrity of the dry dock entrance, walls and floor than at present. It may be necessary to take invasive measures aimed at investigating the under-wall and floor structures, and at ensuring the ship's support structures are adequate.
- 38.3. Second, that the conservation needs of the dry dock as a listed structure, should be considered. Any treatment designed to preserve the ship must be carefully considered as to how it will affect the dry dock. The conservation needs of the dock itself will need to be met through detailed analysis of the dock structure and condition, including photogrammetric survey and photography, and non-invasive survey. This should include preliminary cleaning to enable a more comprehensive survey, removal of all organic matter & litter, raking out joints, re-pointing using an appropriate mortar and resetting loose stones & bricks. A regime of maintenance cleaning and repairs will need to be established.
- 38.4. Third, that full, safe public access to the dock, both to view the ship and to experience the dock must be made. A visit into the dry dock is considered by the ss Great Britain Project as an essential part of the visitor experience to the ship. Further work will be necessary to bring the dock up to an acceptable standard to allow the extension of safe public access beyond the currently restricted area. This will include creating elevator access and ensuring floor and wall surfaces are suitable.

39. Recommendation 10 The Caisson

- 39.1. The caisson must be inspected and treated in a manner agreed with the curator. It is important that the caisson should continue to perform its function correctly. Any treatment should ensure continued structural integrity and that the sluices open and seal correctly when closed.
- 39.2. Inspection and treatment can only occur if a temporary dam is constructed between the Floating Harbour and the caisson that will allow the water between the dam and the caisson to be pumped out. The caisson could then be lifted out using a mobile crane.
- 39.3. This should be done by constructing a sheet piling dam across the entrance to the dock. This would have a number of advantages:
 - 39.3.1. the sheet piling would act as a physical barrier and protect against catastrophic failure of the caisson;
 - 39.3.2. the water between the new barrier and the caisson could be pumped out periodically to allow inspection and maintenance of the caisson. This pumping system could form part of an improved waste water management system;
 - the caisson could be lifted out of position and taken away for treatment, if necessary;
 - 39.3.4. the caisson, dock seals and surrounding masonry could be more effectively treated;
 - 39.3.5. the dam could form an anchor for a new pontoon allowing pedestrians to pass along the towpath across the dock entrance.
 - 39.3.6. the dam could be removed at a later date if required.
- 39.4. In the short term, a boom or very strong and firmly anchored chain should be fitted across the entrance to the dry dock.

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Acknowledgements

Considerable help has been offered and gratefully received during the preparation of this report. Thanks are due to:

Maurice Ball ss Great Britain - Engineering volunteer

Des Barker Portsmouth University - Lecturer in Corrosion Science

Roger Barnes ss Great Britain - Engineering Chargehand

Joe Blake ss Great Britain - Initial Director

Barry Bromley Quantity surveyor Stewart Bowler SGB Major Projects

May Cassar Museums & Galleries Commission
Shane Casey ss Great Britain - Curatorial Assistant
Simon Clarke Sandberg Consulting Engineers
Dr Ewan Corlett ss Great Britain - Vice President

Dr Jo Cox Keystone Historic Buildings Consultants
Julian Harrap Architects

Julian Harrap Julian Harrap Architects
David Hill South West Museums Council
Martin Holden Holden Conservation

Martin Holden Holden Conservation
Des Jarvis Leighs Paints

Peter Lawton Hampshire County Museums Service
Bob Mealings Royal Naval Submarine Museum

Peter Meehan Science Museum, Wroughton - Head of Conservation,

Brian Morton The Morton Partnership Ltd.
Edward Morton The Morton Partnership Ltd.

Frank Porter ss Great Britain - Engineering consultant

Steve Proud Hodge Clemco Ltd.

Simon Raeburn - Ward Interface Force Measurement Ltd Nugmais ul-Rasheed Acrylon - tannate treatment

Claire Smith University of Cardiff research student

Rebecca Stevens ss Great Britain - Volunteer

Siobhan Stevenson University of Cardiff Senior Lecturer

David Stirling
Matthew Tanner
Robert Thorne
Ann Towers
Jonathan Walton
David Watkinson
Duncan Wilson

Mowlem Civil Engineering
ss Great Britain - Curator
Alan Baxter & Associates
Julian Harrap Architects
The Severn Partnership
University of Cardiff
Inskip & Jenkins Ltd.

Chris Young ss Great Britain - Curatorial Assistant

Jean Young ss Great Britain - Archivist

Andrew Wood ss Great Britain - Curatorial Assistant

Lindsay Ward ss Great Britain - Volunteer

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Appendix B

Brief for Conservation Consultants ss Great Britain Project 1998

ss Great Britain Project Brief for Preparation of a Condition Report for the ss Great Britain

1. Introduction

- 1.1. A Condition Report is a document that states what is the current chemical, physical and biological condition of the original fabric of the iron steamship, ss Great Britain.
- 1.2. This report is integral to the work carried out under the main Conservation Plan, but it may be viewed as a separate project where the skills of another consultant(s) or sub-contractor are seen as necessary. In either case, this report must be dependent upon the findings of the main Conservation Plan.

1.3. Commissioning body

- 1.3.1. This Condition Report is commissioned by the Executive Committee of ss Great Britain Project Ltd.
- 1.3.2. ss Great Britain Project Ltd. is a company limited by guarantee for the purposes of preserving and displaying for the public benefit the ship ss Great Britain within her original building site, and is located at the Great Western Dock, Bristol, BS1 6TY.

2. Definition of place or object

2.1. The Condition Report will examine the ship known as the ss Great Britain, which is defined as the ship created by I.K Brunel and his collaborators and launched in 1843, until the end of her working life as a ship, hulk or wreck in 1970.

3. Purpose of report

- 3.1. The purpose is to provide a report of condition, evaluate the report, and consequently to recommend possible conservation solutions. These solutions must accord with the requirements for the retention of the significance in the ship outlined by the main Conservation Plan for the ship.
 - 3.1.1. The report will describe the current physical, chemical and biological state of the original fabric of the ship.
 - 3.1.2. The report will provide an evaluation of the current state of the fabric, and provide a prognosis for the proceeding future condition of the fabric.
 - 3.1.3. The report will provide consequently, in consultation with the curator, a statement of options for specifications for possible conservation solutions.

4. General parameters, time, scale, and remuneration

- 4.1. This Report is jointly funded with the Heritage Lottery Fund, who have also assisted with the appointment of a professional curator to ss Great Britain Ltd. The consultant(s) will be expected to liase closely with and work in conjunction with the curator at all times, and the curator will be the point of contact between the commissioning body and the consultant(s).
- 4.2. The Condition Report will commence as soon as mutually agreeable after the approval of this brief by the Heritage Lottery Fund Project Monitors. A timetable for the work will be agreed with the curator based upon the following stages:
 - Draft of report on state of original fabric
 - Comments upon report
 - Draft evaluation and prognosis report
 - · Comments upon report
 - · Draft statement of options

- Comments upon statement
- · Submission of completed final report
- 4.2.1. The consultancy fee will be agreed and paid on invoice at the submission of the final report, or at other intervals to be mutually agreed.
- 4.2.2. All analysis must be based upon evidence, which should be properly referenced.

5. Publication and Copyright

5.1. Copyright will remain with the author(s) of the Condition Report, but the author(s) must agree to the unrestricted use of the material by the commissioning body. The author(s) will be expected to co-operate in the publication of a mutually agreed text of the Condition Report.

5.2. Presentation

- 5.2.1. The final report should be produced in four copies bound in A4 or A3, and a further copy on computer disk.
- 5.2.2. All terminology used in the report should be based upon the agreed terminology found in the Burra Charter, and amplified by Kerr (The Conservation Plan, 1996).
- 5.2.3. All expenses involved in researching, producing and presenting the report should be included in the tender price.
- 5.2.4. A formal presentation is not envisaged since close liaison with the curator is expected throughout the course of the work.

6. Indemnity

6.1. The consultant(s)s must agree to indemnify ss Great Britain Project Ltd. from and against all liability in respect of personal injury (including death) to persons including the consultant(s)s, or damage to property arising directly or indirectly out of any act or omission of the consultant(s)s in the course of carrying out the services described in this brief.

7. Role of ss Great Britain Project Ltd.

- 7.1. ss Great Britain Project Ltd. will:
- provide access to its staff and advisers at mutually agreeable times.
- provide access to all relevant documentary material in its possession or collections.
- provide access to the ship and all appropriate spaces at mutually convenient times.
- provide a full briefing on the general outline of possible desired developments and alterations to which the ship may be subject.
- provide any other assistance by mutual agreement.

8. Condition report on the state of the original fabric of the ship

8.1. The consultant(s) is to examine, photograph, and describe in an appropriate manner the evidence which remains within the ship for her current condition

8.2. Existing work carried out, particularly by Dr Ewan Corlett (The Iron Ship 2nd ed. 1990), will give a strong lead to understanding the history of the fabric of the ship. It is anticipated that Dr Corlett may make himself available to advise the consultant(s) carrying out this work. Investigation of archaeological or physical evidence should not involve intervention in the surveying fabric of the ship, unless a good and pressing argument for such work can be sustained.

9. Evaluation and prognosis of condition

9.1. The consultant(s) is to gather and reference all documentary information that can be used to understand the progressive history of the condition ship and her individual parts and other features. ss Great Britain Project Ltd. possesses an incomplete set of plans, photographs, reports and references to the ship.

9.2. Physical condition of the place

9.2.1. The consultant(s) is to provide descriptions of the physical and structural integrity of the ship sufficient to enable policy decisions to be made on appropriate treatment of fabric, and to call attention to areas where more detailed or specialist survey and investigation may be required. These might include survey drawings, architect's inspections, structural inspections, specialist surveys such as condition reports, M & E inspections, and health and safety requirements.

Appendix C

Tabulated results of ss Great Britain acoustic and visual test programme
Eura Conservation 1999

Condition of hull plates

	T	ercentage of	sites tested for categories 1 -		in :
Condition of pla (see below)	te Port :	Port external	Starboard Internal	Starboard external	Total.
4	23	5	25	4	17
3	41	54	40	42	44
2	17	37	21	53	28
1	4	3	3	1	3
Areas examined that were wholl composed of GR or covered with timber or concre	y P,	1 .	11	01	8
Condition 4	Very Poor, dis become lace-l	splaying very se ike or entirely n	vere corrosion wit on-existent during	h parts missing. dry abrasive cl	Will eaning
Condition 3	Poor Conditio perforated dur	n, displaying se ing dry abrasivo	vere corrosion and e cleaning	l likely to becom	ne
Condition 2		n, corroded with dry abrasive cl	some probability eaning	of a reasonable	amount of
Condition 1	Good Condition	on, with a strong	g probability of a r	easonable amou	ınt of iron

¹ This does not imply that there are no fibre-glassed areas on the exterior, merely that problems of access precluded examination of those areas. A large number of fibre-glassed areas were examined from within the hull.

surviving dry abrasive cleaning

Acoustic and visual examination of hull plates - Port, internal

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Acoustic and visual examination of hull plates - Port, internal

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Acoustic and visual examination of hull plates - Port, internal

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Acoustic and visual examination of hull plates - Port, external

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Acoustic and visual examination of hull plates - Port, external

Frame	法處	EL SE	10 (C)			SEP. 10		trake	(numb	ered 1	from 1	the weather deck down)
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99						-		- 1				i4g i3g i2 i3 i3h i3 i3h i3
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07		T	1				1	_	-	-	-	h 2 2 3
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	110			53g	i3 s3	i3g	i3g	13g	12	i2	12	
	i2		s2	s3	1830	i2	ii2	13	12	112	12	i3 i3g i3 i4g i2 i2 i2 i2h
	12		3g	-	s3g	li2g	13	13		i2	12	
				s3g		i2	12	ii2		12	12	i2 i4g i3 :i4g i4g i2 i2 i3h i3 g i3g i4g i3h i2 i2 i2

Acoustic and visual examination of hull plates - Port, external

Frame Number from	Weather			1000		74		30	F van				(12.50) (12.50) (13.50)	k down			144	467	10.00 10.00		
perpendicular.	deck	2	3	200	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	kee
132	- TANKE	li3g		152	is3g	1830	113	!i3	i3g	13	112	112	ji3	li4g	!i4g	113	:i3h	112	12	12h	
133		i3g	g	152	52	s3g		i3	i4g	i4h		12	112	li3g	13	113	13	12	:12	13	
134		i3g	lg	s2	s3	s3g		13	i3	12	1			9	i4g	:13	13	:12	i2	12	
135		i3g	g	s3g	s3g	s3g	112	i3g	i2	12				9	l4g	i3g	i3	i2	i2	i2h	
136		ii3g	g	s2	530	s2	12	i3	12	12	1		1	149	li4g	13	13	12	įi2	13	1
137		i3g	g	:s3	13	12	12	i3	i2	i2	1					13	13	13	li3	13	
136		li3	g	s3g	s4h	s4g	12	12	12	i2				1		ii4g	ii4g	13	i3	12	
139		13	q	s2g	i3g	i4g	i3		13	li2						i4g	14	13	i3h	12	i
140				1			T							1			149	13	13	1i2	
141														1		1	113		li2h	i2	1
142							-								1		113	ji3		12	
143	-															1	:i3h	113	13	i3	
144			T					8									i3h	13	13	i3h	
145													1		S		i3	13	13	i3	
146				1										1						13	
147										1. 1	9						į.	i3	13	12	
148																			13	i3h	
149			1																113	i2	
150						- "													13	i2	1
151		1											i					li3		12	
152																	1	13	13	12	
153	S						Section 1												13	i3	
154									J								-			13	
155									J. 13											13	
156																				i3	
157					7000	11111														13	
158																				13	
159																	1		i3	13	
160									English .			0.655				Valencial III			14	13	
161						113					-						1			ğ	

Acoustic and visual examination of hull plates - Starboard, internal

Number from			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	MARK.	22	NA.		The state of	nbered	om th	e we	ather c	leck do	(nwn		100-10	1		4
Aft	Weathe	A SECTION AND A		10,100	S SOL	HERES.	The state of		COLUMN TO SERVICE SERV		言語				140	ACLAND.			愚
perpendicula	deck	2	3	4	5	100	特的	75.16				EL PAR			#2	独てお		7572	惠
-5		1	1		2	0	DR. CR	.8	9	0 1	1000	2 1	3 1	4	15	16 1	7 10	O PULL OF	
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-3	Is2	1549	g	9			-		- 1			1							
-2	is4g	1849		1	1	-	-	-	_	-	-		C (2)	1	1			7	-
-1	s4g	9	i4g	1	-	+	-	+		-					1			-	-
0	1549	9	9	1	- 1	1	-+	-		1	1	1	1		-				-
1	Is4g	s4g	i4g	-	1		+	-		1	1			1	1		-		
2	s4g	54g	g	1	-	-	-	-	-	1 -	-	1				1	1	-	-
3	s4g	s4g	si?4g			-	-+	+	-i-	-	-	-	1		1	7	1	-	-
- 4	s4g	s4g	s4g				-	-	-	-			1		2		1		
	s2		9	- 1		1	+	-	-	-	-	1							
	53	s3g	S3			1	1	+	-	-		1		1			-		-
	s3	g	s3g				-	-	-	-		!	1				1		*
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9			1	/s3			+	+		-		113	51	-52	149	113	41	-	
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12				54					-					13	113	-	i4g		_
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14				s2	i2	i3	li3g	13	1	-			_		i2		i1	 -	
15		-		s3g		i3g		lig	-						13	-	i4g :		
				s3	112	i3g	19	12	-	Įį.	_				13		12		
17				64	12	i3g	g	i3	1-						14		2		-
19		_		/s3	13	13	g	i	1 1	ir	_						3		-
20						1	1	1	1	in	_	2g i	-		i4g		3	;	
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28		-	-				100		in		13		/14	-		-		1	1
29	-	-	-	-				1	Inv		112	112	12	12	-	g inv		i	1
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34		+	1-	- !	- !				nv	12	12	li2	13	1139			1		
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6	-	+			3 1		49 19			13	112	:13	li3g	113	1140			-	
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9		T		3 5	-		-		nv	i4g	i4g	i2	1i2	13	nv	nv	1		_
0		1		3 5		-	-		-	113	i4g	i4	i3g	ny	inv	inv			
		1		3 12		-	Transport of the last		nv	14	li4g	149	ii4g	13	inv	nv	-		_
	-		is		I There is no case	13	minute process	9 13	inv	113	i3g	13	13	14	nv	nv	1		
			S				The state of the last	100	inv	:13	13	13	13	113	i4g	inv	1-1		
			S			13	-	12	114		13	113	ji4g	13	inv	inv	†		_
	_ !		S			140	13		113		13	13	14	i4g	Inv	inv	1	-	-
			s.	_	12	Inv	140	-	inv	13	13	13	i4g	i3	nv	ny	1		U
			154		i4g		Inv								1	1	1 +		-
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\$4g	s4g s		152	li3	13	nv	1000		13 1					- 1		T			1
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18.5	149 14	9 52	s2									- 1	1	1			-		
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Acoustic and visual examination of hull plates - Starboard, internal

- DEFE		Total Control	対象を		1173		Str	ake (n	umber	ed fr	om the	weat	her de	ck dow	m)	蠹				
Frame Number from	全门	(Trips	Table 2	交通数		The state of	9854	Auto Carlo	7.256	5	300 OM	1		Test	E.F	V.	南韓	As E	10.5	100
Aft	Weather	1256	OPPECT POSTE	SHIP	A STATE OF	200			Francis No. 10	1	TE NO	MORNING MORNING	-013	30 00 00 00 00 00 00 00 00 00 00 00 00 0	Carries Carries		Cont.	EL TOUR		Sales
perpendicular.		2	3	255	5	- 6	JU19	8	9	1	0: 11	12	1	14	1!	16	1	7 18	19 20	ke
63	s3	\$49	is3	s2	s2	i4g	inv	inv	i3	li2	įi3	13	149		1_				<u> </u>	<u>.i.</u>
64	s3	Js2	s2	nv	s2i4	g i4g	13	nv	12	112	113	114	113	13	i3	149	13	·i4g		
65	53	is3g		nv	i4g	i4g	li4g	149	112	li2	13	113	113	li3g	113	113	:9_ 14	nv		
66	52	is3g	-		i4g	li4g	113	113	12	li2	12	13	12	113	12	113	:14	19		
67	54g 54g	52	s2 1g s1	I3 S2	i4g	i4g	14	INV	li3h	12	12	12	13	Ti3g	14	113	149	g	 	
69	s3	s4g		53	1149	140	i4g	14	112	ii2	13	13	13	113	112	113	113	gh		
70	nv		52	inv	151	li3	13	14	ıs3g	s2	s 2	l3h	52	13	li3	113	13	ii4g		
71	s4g	s4g		s1	s1	il4g	13	13	13	li3	l3	113	i3	ii2	112	i3	i3g	113		
72	s4g		152	151	ls1	13	12	12	14	113	i3	13	13	12	!13	13	13	13	·i	-
73	s3		52	IS1	s1	13	13	13	12	13	ii2	!nv	nv	9	C	ic.	·c	ic		
74	s4g	549		151	51	14g	i3 i4g	i3 i3h	i3	13	i2	13	13	113	ic li3	C	C	ic		
75 76	s3 s3	is4g	-	151	51	i4g	i4g	14	i3	112	13	113	13	12	113	130	13	19		
77	s3	9	9	s1	s1	13	i3	li2	i2 .	li2	13	114	inv	12	12	li3	13	113		
78	s3	549		s1	51	149	Inv	13	112	112	li2	13	li3h	li2	112	li3	113	13		
79	nv	s3	s4g	nv	s2	13	nv	13	s2	52	52	s3	is4g	i2	i2	li3	13	113		1_
80	s3g	s4g	9	nv	s3	13	nv	13	162	52	13	13	13	112	13	113	li3g	12		1
81	52	s4g	9_	nv	s3	i3	inv	13	s2	52	s2	i3g	13	12	i3	1i3	113	13	i -	+
82	s3	9	9	nv	s4g	12	i2	13	-	-		-	-	13	12	13	i3	13		
83	nv s2	s4g s3g	9	nv	s4g	i3 nv	nv	nv	1	+-	+-	1	16	13	13	13	12	13		1
85	nv	53g		inv	1	ii3	nv	nv	1	1	1	1	i	12	13	13	i3	lia ,	- 1	1
86	nv	s3g	is3g	inv	s4g	13	14	i4g		L		1		i3	i3	i3	i2	13		1
87	nv	s3g	s3g	nv		12	13	13			î.		1	li2	112	12	12	i2		1
88	s3	i3	i4g	nv	14	13	li4g	li4g				1	1_	li3	li3	13	114	ii3		-
89	s2	52	s3g	nv	149	i4g	3	113	-	-	-	1		-	1-	1	-	-	i	1
90	52	14g	9_	nv	149	i3g	1149	i4g	-	-	-	-	-		+-	+	-		-	1
. 91 92	~			+	9	9	i3g	9	-		-	!	-	-		+	-	-		+
93	Gangway	i iii	ive.		i4g	i4g i3g	149	13	1	+	+	1	+	•	1	†	1	7	+	1
94		t		1-	62	i3g	i4g	140		1		-	1		1	1"		1		
95	52	s3	s4g	nv	s1	i4g	li3	i4g									1			1
	s2	s4g	s4g	nv	st	12	i2	i3g		1	1	1	1	<u> </u>	1		1	-		
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	nv	i4g	i4g	inv inv	+-	-				-		+	-	-	+		1	1		T
or i rem to atherm mand	nv		s4g	nv	+		-	·	-	-					†	1	1	1		1
THE RESERVE AND ADDRESS OF THE PARTY OF THE	nv		1549	Inv	1					-	1							1 1		
and the second second	nv		152	nv	1													1		
104	ΠV	:549	s4g	nv													<u>. </u>			1
	nv	:s3g	s4g	nv			_				1			1		-	-			-
	nv	Is4g	and the Person	INV	Me	Me	ide	ia	13	14	13	13	12	i2h	nv	inv	-			i-
THE RESERVE OF THE PARTY OF THE	i4g i4g	i4g s2	s1 s1	s3 s3						13	13	12	112	**********	Inv	C	-			İ
Andreas Company of the Parket	3	162	52	s3	52					13	:13	13	13		ііЗс	C	С	c		
minutes / management and	i3	51	s1	52	der vierten	the otherwood				13	i3	12	ii2			C	C			
	s2	s1	st	1	1			the State of Street, or other Designation of the last	-	i3	li4	13	-		C	C	C	С		-
	49	9	st	1				_		13		-	posts yourself set	12	_	-	i2c	C		
	s2	g	51							13		12	annual memory	12	-		i2c	C		-
	3	149_	51	-						13			13	-	i2c		i2c	ic	-	
	52. 52	s1 s2	s1 s1					i3		13		PER SAMPLE TOWN		i2	i2c			c		
	52	52	52	-						13	140	-	the same and		li2		12	c		
	53		s1					-		13					i2c	i2c	i2c	С		
	52	s2gh		s 3	14 g	i4g	* * * * * * *			12		12	13		i2	i3c	іЗс	i3c c		
120	\$3	i4g	s3	149		i4g	13	13		12	the second				i2			C C		
	3	s3h		i4g				and the same		13				ACCRECATE VALUE OF	Trib Street	-		C		_
	3		s3	14			11.00			13	delicated and the	-			12		_	i2 c		
	3		14				confinement			62		-		12	-	Assert Court	c c	C C		-
	3g			13						s2 i3			14		ACCRECATE VALUE OF	-	c	c		-
	:4g :3	m			i4g i4g			i4g is?4		s3		2		an obstance				c	c	
					i4g	49	a collection			13		12	i3	and which seems	terms to make	4000		c c		
		-								s3					i3	12	c	c c	and it make province the same of	
						-				13		13				1710		13c c		
	2	s3						i4g		13				-	-		i3c	C		
										13					CO Primary	-	nv	nv n		
132 5	2	s3gh	i4g .	53	i3 !	s3	4	i3 (i	4	13	13	s3	12	13	13	nv i	nv (nv in	V /	

Acoustic and visual examination of hull plates - Starboard, internal

Frame Number from Aft	n Weath	er					S	rake (numt	ered	from t	he we	ather	deck d	town)						
perpendicula	deck		2	3	r Bereye A Silence	5	В	1997		FFRIER			Day at			7 diretr				20.2	Min I
133	s4g	sa.	the same of the last		-	Complete Street	1019800-013	13	white the	Name and Address of	Section		The second second	13	14	15	16	17 1	8 1	9 2	0 kee
134	s3	. \$2	and yet miles in	-				-13	13	14	-	Committee of the	-	113	130	c in	v 'r	w inv	inv	1	- nec
135	53	182		140				_	s3			14	-	12	13	n	v r	v nv	Inv	****	
136	183	154	54		-			140	more as I	-	:s3	-		113	1131	7 -0	v n	v inv	Inv		-
137	s 3	140	h li4	84	Tree her seeds			_	i3	113	14	14		113	: i3c	: in	v n	v 'nv	nv	014m + +	* **
138	63	13	13	-54	.140	i4g		13	140		13	12	13	13	i2	13	c n	v nv	inv	nv	* **
139	ii4g	149		140	149	1149			113	113	130	-	:13	14	i3	13	12		THE RESERVE	nding	water
140	i4g	149			140	140		149	i4g		:54		-	113	:i3	;13	.12	12	12		
141	.s3	is2		inv	i4g	149	g	14	i4g		- 0			114	13	113	13	nv	inv	nv	***
142	st	s2	152	inv	1140	140	i4g	ii4g	149	ii3	149	140		ii3g	13	12	-12	nv	nv	nv	
143	İst	1s2	53	Inv	149	The books	149	ii4g	149	ii4g	149	149	_	113	139		1 113	.nv	·nv	nv	··
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Acoustic and visual examination of hull plates - Starboard, external

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Acoustic and visual examination of hull plates - Starboard, external

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Acoustic and visual examination of hull plates - Starboard, external

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Appendix D

Preliminary Survey of the Great Western Dry Dock and other masonry. Ref 418 Holden Conservation, 26 November 1998 In the following text references to the "dock" should be taken to include the historic walls including the brick wall currently bounding the stern of the ship and the stone walls forming part of the area used by the wood yard. When reference is made to the "dry dock" this refers to the area which floods to allow the ship to float.

For convenience at this stage no distinction is drawn in the importance of the different areas although later on within the project distinctions in the manner of treatment may be necessary to allow development in the complex. For instance the boundary walls may require more restoration to ensure public safety or to provide security.

SURVEY AND BRIEF.

A visit was made in May 1998 to visually survey the dry dock and surrounding dock area of the SS Great Britain.

The purpose of the survey and the following report is to provide some general comments on the issues involved in the conservation of the stone and brick fabric with in the site.

The intention at this stage is to provide an overview and make suggestions for work that should be included within the main conservation project.

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Outline for further documentation.	page	3
Outline for further condition survey.	page	5
Brief summary of the current condition	page	7
Examples of possible conservation	page	8

3

DISCUSSION OF THE CONTEXT

The dock is the environment for the ship. Consideration of the dock can not occur without account of the requirements of the ship.

The dry dock and the surrounding dock land provides the context for the ship. It will be crucial to preserve the context.

Any intervention on conservation grounds must be carefully considered with in the overall context.

So for example:

the dry dock would almost certainly always have been damp with water seeping in and rain being accumulated, to set an objective to dry the environment would constitute a change in the historical and current context.

It may eventually be decided that it is necessary but the justification for doing it must be considered against the destruction of part of the context.

This is only an example and may be neither possible nor required but it does illustrate the delicate conservation issues which go beyond technical matters alone.

To continue using this example the complications in drying the environment may require intervention within the dry dock structure which would destroy historical or archaeological information.

To understand and assess the present state of the archaeology is considered a primary objective which would allow for making informed decisions about any conservation measures that may be required.

To this end the first aspect of the conservation recommendations is to set out the nature of further documentation and analysis.

OUTLINE FOR FURTHER DOCUMENTATION

This should be compatible with documentation systems to be used elsewhere in the overall project.

Detailed analysis of the current structures and condition is required.

For this;

- 1. All areas of the dock must be photographed in detail on a grid pattern. The exact requirements need consideration but it is suggested that the grid be in approximately metre square sections.
- 2. photogrammetric survey to be undertaken and a full set of drawings produced for use in documentation. The scale should be relatively large to assist in accurate and detailed documentation.
- 3. Produce a number of cross sectional surveys through the width and the length of the dry dock.
- Consider the use of a metal detector scan of all areas to ascertain the presence of buried metal which may possibly be constructional cramps.

To facilitate the photography and the photogrammetry it is recommended that the surfaces are first cleaned to remove organic growths and general soiling.

Analysis.

- 1. Undertake a preliminary visual survey to identify the different types of stone, mortar and other materials used in the construction.
- 2. Record the findings on a set of drawings and agree the location and number of samples to be taken for geological and material identification.
- 3. Take samples for
- geological identification and possible tracking back to quarry
- materials identification /
- mortar analysis /
- metals analysis /
- timber analysis

Analysis would provide the following information;

- If the sources of stone are identified historical information about the quarries may inform the knowledge about the periods of construction.
- The presence of other materials with in the construction may also add to the understanding of the periods of construction.
- The dry dock is from a period in history when hydraulic mortars were developing rapidly and much information of interest may emerge adding to the body of knowledge.
- Plotting the use of the different mortars may identify different periods of building and maintenance more accurately than the types of stone which could easily be reused from earlier construction. There may be links established between the dry dock and other walls on the site.
- If mortars need to be repaired the analysis will be crucial in developing suitable
 matching repair mortars. Note that the brick wall at the stern of the ship was
 originally built with a black mortar (photographs 32,33,34,35).
- Identification of the various metal inserts around the dock may help to provide information about the use and date of manufacture.
- The various bulks of timber where they are built into the structure of the dry
 dock should be identified to assist in preparing their conservation requirements.

Following the analysis:

- Record the results of analysis on sets of drawings and apply the results of the samples to code the different areas with materials, construction methods and possible dates or relative periods of building.
- Compare with other docks, dock walls etc. either in the locality or with other historical docks.
- Document the masonry techniques.

Identify types of cutting, methods of working stones, tool markings, methods of construction and other information which will help to identify similarities and differences throughout the dock. This may provide information about the sources of material and identify different periods of construction.

OUTLINE FOR FURTHER CONDITION SURVEY.

A full survey of the condition should be undertaken before any decisions are taken about the details of any conservation programme.

A very detailed survey is necessary to establish a conservation management plan.

To enable the survey to be properly undertaken the surfaces should be cleaned to remove organic growths and soiling.

The condition survey of the dock must encompass the visible surface material and the substrate. Consideration should be given to the use of non invasive survey techniques where ever possible. Invasive techniques may be employed where the perceived benefit is deemed to be greater than the damage caused to historical material.

Non invasive survey.

A set of drawings should be annotated with;

the condition of the structure in general including cracks, settlement and alterations to the historic construction.

the condition of each stone, brick, or other components detailing cracks, friability, organic matter, rot, and other items pertaining to their past, current and future conservation.

the presence or absence of mortar, its condition and an assessment of its ability to function appropriately within the construction.

presence of metal inserts (pipes, rings, cramps etc.)

the condition of the timber used in the construction.

Use of non invasive archaeological methods such as ground radar may provide information about buried structures around the dock environment. It may also help to ascertain the sources of water seeping or flowing into the dock.

There may be other methods not known to the author of this report.

Invasive survey.

Consider whether it is necessary to undertake investigation of the substrate by opening up the construction.

for the purpose of adding to the information about the methods of construction and to compliment other knowledge of the archaeology of the dock.

for structural or engineering reasons it may be decided to investigate areas of water seepage.

Where this occurs careful documentation of the removed materials will enable precise reconstruction.

BRIEF SUMMARY OF THE CURRENT CONDITION.

Dry dock

The condition of the stones within the dry dock is generally good but the condition of the pointing gives cause for concern.

There has been a history of repairs which needs further study but in general it is anticipated that patches of recent hard cement pointing and render will need to be removed as it appears to be failing. See photographs numbers 9 and 10 where recent "ribbon" style pointing is shown to be cracking and falling out.

Boundary walls.

The condition of the stone within the boundary walls is also generally good but the pointing is badly in need of maintenance.

Brick wall.

The brick wall at the stern of the ship has been made from quality bricks which remain in good condition. It was originally constructed from a black mortar which has been over pointed with a grey portland cement mortar.

EXAMPLES OF POSSIBLE CONSERVATION.

Preliminary cleaning to enable a clearer survey.

Tests should be carried out to ascertain the most appropriate method.

Options are;

remove plants by hands

brushing to remove loose soil from surfaces and joints

hand cleaning of surfaces to remove algae and soil by bristle brush and water or solutions of detergent in water.

high pressure water;

high pressure steam;

Maintenance cleaning;

The dock will continue to accumulate soil and organic growth. Decisions will need to be made about the approach to this. Frequency of cleaning treatments will have implications on the long term conservation of the structure.

Preventive treatments such as applying biocides will impact upon the wider natural environment and present health and safety risks.

Repairs.

To put the structures back into good order a certain minimum amount of maintenance will be required.

This will include;

inspection by an engineer experienced in historic structures to pass comment on the stability, particularly of the boundary walls

rebuilding of loose areas of stone and brick and reintegration of detached components.

consolidation of areas where mortar is substantially lost or failing,

repairs to structural cracks (for example the end wall in photograph

Holden Conservation Ref. 418. SS Great Britain. Preliminary survey. 12/09/98 pointing of joints

removal and replacement of non original pointing which may be detrimental to the long term preservation of the structure

consideration of treatment of integral timbers by consolidation or maintenance of the wet environment.

Establishment of a conservation management plan.

This will include recommendations for maintenance and regular inspections of the condition.

Holden Conservation Ref. 418 SS Great Britain Survey.

Budget costs. Prepared 12th September 1998

1 Cleaning to allow for further detailed surveys and recording. 1a Dry dock take out weeds 2 men X 1 day gentle pressure wash 2 men X 10 days scaffold access pressure wash hire 1b brick wall - no work needed 1c boundary walls remove plants 2 X 1 day gentle pressure wash 2 X 5 days 2 Photographic survey allow for professional photography - complete guess at 3 Photogrammetric survey - complete guess at 4 Preliminary visual survey of material types inc. documenting a set of drawings as provided by photogrammetric survey to determine the analysis required, and take samples in association with specialists. allow 1 X 5 days	2 20 2 10	700
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8 timber analysis		0
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SS	olden Conservation Ref. 418 5 Great Britain Survey. 11 Non invasive condition survey	Prepared	12th		get costs. ber 1998
	recording of condition of individual stones assume only record where problem exists that are not documen the photogrammetric survey and where the photographic record to be supplemented with commentary.	ted by s needs		0 0	
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	ground survey costs - no idea what this might be			5000 0	8"
1	12 Invasive survey			0	99
	allow to open up certain areas			10,000	alis ya barani
				Ö	
1	3 Repairs structural engineer			0 1000 0	¥
13	a rebuilding loose and decayed stone and brick dry dock area			0	
	allow for 20 sq. m. @ £ 400 per metre boundary walls			8000	
	allow for 100 sq. m @ £400 per metre			40000	
13b	consolidation where mortar is lost or failing			0	
	dry dock area allow for 100 sq. m @ £200 per m.			0 20000	
				0	
	brick wall allow for 100% @ £200 per metre sq.			0.	
	what is the length X both elevations			0	
	guessed at 120 metres			24000	
				0	
	boundary walls allow 100% @ £200 per metre sq			0	
	what is the length X both elevations			0	
	guessed at 3000 m sq.		6	00000	
	•			0	* 1
				0	
13c	pointing of joints			0 1	180 PM 4
	dry dock area only (rest is 100% covered under 13 b)			ő	
	allow for 50% of area @ £100 per m sq.			0	
	area guessed at total 4000 sq. m. allow 2000 m sq @ £100		20	00000	
				0	
13d	repairs to structural cracks			0	
	allow a lump sum			2000	
				0	
130	Pomovol of detrimental pointing account of the total			0	
108	Removal of detrimental pointing covered under item 13c		188	0	
	PAGE TOTAL		91	4000	

Holden Conservation Ref. 418
SS Great Britain Survey.

13F Conservation of timber elements allow lump sum amount

PAGE TOTAL

SUMMARY

PAGE 1 PAGE 2 PAGE 3

BUDGET TOTAL

Prepared 12th September 1998

2000

37300 914000 2000

Testing of structural materials ss Great Britain, Report 17499/M/01 Sandberg Consulting Engineers, 2 October 1998.

SANDBERG CONSULTING ENGINEERS

TESTING INSPECTION QUALITY MANAGEMENT

Messrs Sandberg 40 Grosvenor Gardens London SW1W 0LB

Tel: 0171-565 7000 Fax: 0171-565 7100

Email: sandberg@compuserve.com

REPORT 17499/M/01

TESTING OF STRUCTURAL MATERIALS

SS GREAT BRITAIN

Reference: Instruction from Mr R Turner of Naylor Conservation.

1. INTRODUCTION

Site visits were conducted to the SS Great Britain, Bristol Historic Dockyard by our engineers on the 29 and 31 July 1998 in order to remove samples of structural material and assess the load bearing wooden supporting struts. In addition to this inspection and testing was carried out to determine the condition of the coffer dam used to secure the dry dock in which the ship is berthed.

The samples of structural material were tested to determine their mechanical properties and establish a better assessment of the structural performance of the hull including the rivetted joints.

For the purpose of testing the samples were given the following unique reference numbers.

Metallurgy Laboratory		S	Sample Reference	e / Description
Reference	-		1000	No 26
ME 479	BR	SGB	1998	
	BR	SGB	1998	No 40
ME 480	DK	002		No 67
ME 481	BR	SGB	1998	140 07

Additional samples of corrosion product were received on the 1st September and these were given the following unique reference numbers.

Metallurgy Laboratory Reference	Sample Reference / Description				
ME 594	Corrosion Sample	No 2			
ME 595	Corrosion Sample	No 3			
ME 576	Corrosion Sample	No 4			
ME 597	Corrosion Sample	No 5			

2. SAMPLE DESCRIPTION

Sample ME 479 was a large flat plate with a rivetted lap joint along the centre. Both plates were approximately 56" original thickness which was determined from sections of less corroded material around the rivetted lap joint, (see Plate No.1).

Sample ME 480 was a large flat plate, approximately 1" original thickness, with a rivetted strip along one edge, (see Plate No.2).

Sample ME 481 was a rivetted compound section incorporating flat plates and angle sections forming a stiffening rib on the inside of the hull, (see Plate No.3).

From three samples received five separate material specimens were selected for the program of mechanical testing and three rivetted sections were selected for macro examination.

TEST PROCEDURES & RESULTS

3.1 Laboratory Testing

3.1.1 Tensile Testing

From each of the five material specimens, one tensile test piece was prepared and tested in accordance with BS EN 10002:1:1990. The results are shown on Test Certificate 17499/M/1.

3.1.2 Charpy Impact Testing

A set of three test pieces from each specimen were suitably prepared and tested in accordance with BS EN 10045:1:1990. The results are shown on Test Certificate 17499/M/1.

3.1.3 Hardness Testing

Each sample was suitably prepared and Vickers hardness tested in accordance with BS 427:1990, HV30, the results of which are shown on Test Certificate 17499/M/2.

3.1.4 Metallographic Examination

A section from each specimen was mounted in bakelite and then suitably prepared to a $1\mu m$ finish. These were then etched in 2% Nital and examined under the microscope, the results of which are shown on Test Certificate 17499/M/3 to 7.

3.1.5 Macrographic Examination

Three rivetted joints were sectioned, suitably prepared and then etched in 10% Nital for examination. The results are shown on Test Certificate 17499/M/9 to 11.

Tensile and Compression Testing Across Rivets 3.1.6

Three tensile and three compression test pieces were suitably prepared and tested in our universal testing machine. The results are shown on Test Certificate 17499/M/8.

Determination of Chloride Content 3.1.7

The four corrosion samples were submitted to our Chemistry Laboratory and analysed for chloride content with reference to BS 1881: Part 124:1988. The results are shown on Test Certificate 17499/M/12.

Site Testing 3.2

Examination of Timber Support Props 3.2.1

Six timber props, three from each side were examined to determine the load in each prop. A secondary support incorporating a hydraulic ram and calibrated load cell was positioned adjacent to each of the props. Jacking of the secondary prop was continued until the load was released in the original prop. These results are shown on Test Certificate 17497/M/13 and by Plate Nos. 18, 19 and 20 in Appendix B of this report.

Ultrasonic Thickness Survey of Coffer Dam 3.2.2

An ultrasonic survey was conducted on the coffer dam to determine remaining wall thicknesses and condition. The results are shown on Test Certificates 17499/14a and 14b.

COMMENTS 4.

The tensile test results show a range of 0.2% proof stress values of 206 to 269 N/mm² and ultimate tensile stress values of 231 to 365 N/mm². Three tests gave elongation results of 6.0, 11.6 and 6.6% the two samples ME 479-1 and ME 479-2 both fractured outside the gauge length marks. These variable results are typical of a low strength poor quality wrought iron.

The Charpy impact results gave a range of results from 9 to 48 Joules when tested at 20 °C. Due to excessive corrosion pitting over most of the samples it was necessary to produce substandard sized test specimens. If the sub standard sample results are factored to give the equivalent to the 10 mm samples then the results would be higher. This would increase the average for 479-1 to 22 J, the average for 479-2 to 22 J, the average for 481-1 to 39 J and the average for 481-2 to 20 J. This does still leave the only full size set of results from sample 480-1 at an average of 12 J.

Hardness testing on the five samples gave results ranging from 109 to 141 VPN. This is a wide spread of hardness values and be considered typical of those expected from variable, coarse grained material such as wrought iron. This is particularly so for poor quality wrought iron, such as these samples, where the inclusion size and content can influence the results significantly.

Metallographic examination of the five samples showed microstructures consisting of large non-uniform slag/oxide inclusions in a course ferritic matrix. The structures were highly variable and some of the inclusions were very large which makes these materials typical of a poor quality wrought iron.

Examination of the macro sections through the rivets showed elongated slag inclusions in both the plate and rivet material. This would be considered typical for this type of material. In general the rivets were found to be highly deformed conforming fully to the holes in the plates.

In general the corrosion to these samples had occurred on the exposed faces causing massive wasting of the section. This proved to cause problems in selection and machining of samples for the tension and compression shear testing across the rivet samples. Corrosion products were however visible inside the samples between the rivets and the plates as well as between the plates themselves.

The heads form of the rivets varied, samples 479-1 and 480-1 were counter sunk to provide a flush finish. The sample in 479-1 was only countersunk on one side and the other side which had been subjected to higher levels of corrosion and originally a dome head was severely corroded away. The corrosion had also penetrated along the flow lines into the body of the rivet from both sides. At present the cross sectional area of the rivet has not been significantly compromised but the reduction of the dome head would reduce the mechanical strength of the joint.

The sample in 480-1 was countersunk on both sides and the penetration of corrosion into the ends of the rivet was not as severe as on sample 479-1. However there was a build up of corrosion product around the head of the rivet on one side. Due to the expansion of the oxide as it forms it will hold the joint tight. However the oxide is also friable in nature and as it becomes thicker may be prone to releasing the joint with out much plastic movement. This effect will be enhanced by the build up of oxide between the plates that will put further stress on the rivetted joint.

The samples in 481-1 were both typical dome head rivets which had been inserted into poorly aligned plates with punched holes. The degree of fill due to the deformation of the rivet was lower than the other samples. This may be due to the complexity of the joint or because they were but in a difficult position. There is considerable build up of oxide in this joint, the expansion of which will add to the load on the rivets. The head of the rivets are severely corroded with only small overlap at the edges to retain the plates. These rivets had not suffered penetration of oxide into the shank along the flow lines from working.

During the preparation of the macro samples it was found that the samples deteriorated very quickly after being prepared, even before being etched. The surface corrosion that occurred spread rapidly from the areas of corrosion product exposed on the prepared surface of the sample. This rapid deterioration may be due to the presence of corrodents within the corrosion product which both increase the rate of corrosion and draw water from the atmosphere.

The results of the chloride content testing on the corrosion product samples provided show that there were negligible chloride levels remaining in any of the samples received. This very low level of chloride may be a result of the samples being washed in fresh water prior to their removal from the ship if these areas are subject to regular rain washing. This is however unusual for corrosion products on a structure of this type and in this type of location. Where

the samples have been freshly exposed the effects of the chloride contamination are much more apparent by comparison with areas that would be more readily rinsed.

A series of load tests were conducted across the rivetted joints, three in tension and three in compression. The purpose of these tests was to assess the shear strength of the rivetted joints. Problems were encountered in removing samples from the material submitted due to the severe levels of corrosion that were not always apparent until after attempted machining of the material. Of the six tests conducted only two samples failed by shearing through the rivets.

Two of the tensile test specimens failed by tearing of the plate materials around one of the rivet holes. See Plates No.12 and No.13. This was due to the extensive loss of section from the plate material adjacent to the rivetted lap joint.

The third tensile sample failed by the plate material pulling over the corroded head of the rivet see Plate No.14. This occurred due to the extensive loss of section by corrosion which had completely removed the head of the rivet.

Of the three compression test samples two of them failed by shearing of the rivets and one failed by the collapsing of the plate material due to excessive loss of section from corrosion. See Plates No.15, No.16 and No.17.

The results obtained showed large differences with the samples tending to hold together due to the mechanical locking of the plates where corrosion has occurred between the lapped plates rather than as a direct result of the shear capacity of the rivets. In both tests once the initial friction had been overcome the rivets then sheared through at a steadily decreasing load. In both cases, where the rivets were sheared, the maximum load occurred before there was any significant differential movement of the lapped plates. Once movement occurred and the rivets began to shear the load dropped steadily up to final failure.

Testing of the timber props on site found, in general that the props of the port side of the ship were under less load than a number of those on the starboard side of the ship. Of the three props examined on the port side of the ship the loads were found to range from approximately 15 kN to greater than 25 kN. On the starboard side of the ship a number of props were found to loaded to over 30 kN. A number of other props on this side showed significant signs of bowing due to the load applied.

A number of props on the starboard side were positioned with their bases wedged hard against the wall of the dock and the top end wedged under the angle section stiffener running around the hull of the ship below the water line. The props on this side of the ship appeared to be taking greater loads due to local movement of the hull in this area rather than any significant movement of the ship as a whole.

The starboard side of the ship was the most severely damaged with a large vertical tear approximately amidships which had been crudely repaired by plating. In this area there appears to have been some movement of the hull possibly due to creep of the material or distortion due to the increase in weight on the inside of the hull as parts of the restoration to the inside of the ship are undertaken. Distortion was also apparent in this area where the starboard bilge keel could be seen to distort over one of the supports under the ship. This is shown by Plate 20 in Appendix B of this report.

Inspection of the coffer dam showed no evidence of any significant loss of section from the plates forming the main external skin. The coffer dam was found to be constructed with two

distinct levels inside. Below the line of the first two rows of plates the dam was separated from its base by a complete floor with access to the lower level gained through a small hatchway in the centre of this floor. The lower section of the dam coincided with the bottom three rows of plates visible on the outside of the structure.

The upper floor of the coffer dam was found to be in good condition with the paint coating still present on the internal face of the plates. The lower level of the dam showed no evidence of any recent repainting with the entire internal surface cover with a thin layer of corrosion product under what remained of the paint coating. The upper and lower levels of the structure revealed a difference in plate thickness. The upper half showed a plate thickness of around 7.5 mm and the lower half a plate thickness of around 8.5 mm.

The base of the coffer dam was found to be filled with mass concrete to a depth of approximately 450 mm with additional ballast, in the form of scrap metal principally comprising of rail mounting brackets that was also present on the intermediate floor. During the inspection no evidence was found of any water ingress into the structure, the internal surfaces were dry even in the bottom of the dam.

Examination of the outside of the structure could only be carried out on the inside of the dock due to the water level outside. The area examined showed no evidence of any significant corrosion with the paint coating generally found to be in good condition.

A number of small leaks were apparent around the base and sides of the coffer dam where water was leaking around the outer edge of the structure where it seals with the dock wall.

Naylor Conservation Unit H3 Halesfield 19 Telford Shropshire TF7 4QT

For the attention of Mr Robert Turner

MET/NAF/BRW/gdt/brw

for Messrs Sandberg

B R Whitney

2 October 1998

Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report. Your attention is drawn to the enclosed sample retention form and we would be grateful if you could complete the form and return it within one month from the date of the report.

Tests reported on sheets not bearing the UKAS logo in this report/certificate are not included in the UKAS accreditation schedule for this laboratory.

Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.

CONSULTING, INSPECTING AND TESTING ENGINEERS MECHANICAL TEST CERTIFICATE

Naylor Conservation

Client:

Telford, Shropshire

TF7 4QT

Halesfield 19

Unit H3



Telephone 0171 565 7000 Facsimile 0171 565 7100 10 Grosvenor Gardens Metallurgy Laboratory London SW1W OLB

17499/M/1

16-17.09.98 Test Date

Samples Received 30.07.98

Order No.

Test: Tensile Testing in accordance with BS EN 10002-1:1990

20 20 20 20 Temp 20 Nominal 300J Impact Energy 10 29 12 Charpy Test 11 8 *2 48 18 21*4 11 11 13*2 10 13 12*3 11 10*2 Impact 10 10 Area Reduction 8 Elongation 11.6 6.6 6.0 + -% N/mm² Stress 294 365 312 296 231 Ultimate Stress 30.9 22.3 90.6 47.2 23.2 Load Stress N/mm² 229 248 269 219 206 Proof .oad 0.2 24.1 71.4 16.4 34.9 20.7 Z 105 61.1 288 159 100 mm² Area 6" x 3" Angle section Sample Ref: Specimen Identification ½" Plate, %" Plate 5/8" Plate 1" Plate Met Lab Ref: ME 481-2 ME 481-1 ME 479-2 ME 480-1 ME 479-1

No elongation recorded, samples fractured outside gauge length marks Specification: N/A Comments:

Substandard Charpy impact specimens 10 x 7.5mm Substandard Charpy impact specimens 10 x 5mm Standard Charpy impact specimens 10 x 10mm *3 *

2 October 1998

OB R Whitney Report Date

Specimens will be retained for 2 months unless otherwise notified to the Laboratory

1.3. 00

9

Signature

LAB FORM No. MET/105/B

....

Secretive

CONSULTING, INSPECTING AND TESTING ENGINEERS



No. 0957

Metallurgy Laboratory 40 Grosvenor Gardens London SW1W OLB Telephone 0171 565 7000 Facsimile 0171 565 7100

17499/M/2

Test Date 17.09.98

Samples Received 30.07.98

VICKERS HARDNESS TEST CERTIFICATE to BS427:1990

Client: Naylor Conservation

Unit H3 Halesfield 19 Telford, Shropshire

TF7 4QT

Order No.

Met Lab Ref:		ME479-1	ME479-2	ME480	ME481-1	ME481-2
Client Ref:		%" Plate	5%" Plate	1" Plate	6" x 3" Angle	½" Plate
Load/kg		30	30	30	30	30
Hardness Values	1.	130	123	135	143	127
4.	2.	115	109	141	140	121
	3.	120	118	141	135	109
Average Hardness Value:		122	117	139	139	119
Correlated Approximate Tensile Strength (N/mm²)						

2 October 1998

Report Date

Signature

Specimens will be retained for 2 months unless otherwise notified to the Laboratory

Comments:

CONSULTING, INSPECTING AND TESTING ENGINEERS



Metallurgy Laboratory 40 Grosvenor Gardens London SW1W OLB Telephone 0171 565 7000 Facsimile 0171 565 7100

17499/M/3

Test Date 16-17.09.98

Samples Received

30.07.98

METALLOGRAPHIC EXAMINATION CERTIFICATE to BS4490:1989

Client: Naylor Conservation

Unit H3 Halesfield 19 Talford, Shropshire TF7 40T

Order No.

		M479-1		Client/Ref Description:		등" Plate	
Met Lab Ref:	= 2.5				2% Nital	Grain Size Index:	111
Plate No.:	1	Magnification:	X100	Etchant:	2% NITA	Grain -	

Sampel ME479-1 etched in 2% Nital showing a microstructure consisting of large non-uniform slag inclusions in a coarse ferritic matrix typical of a poor quality wrought iron.

2 October 1998

Report Date

Signature

OOB R Whitney

Specimens will be retained for 2 months unless otherwise notified to the Laboratory

CONSULTING, INSPECTING AND TESTING ENGINEERS



Metallurgy Laboratory 40 Grosvenor Gardens London SW1W OLB Telephone 0171 565 7000 Facsimile 0171 565 7100

17499/M/4

Test Date 16-17.09.98

METALLOGRAPHIC EXAMINATION CERTIFICATE to BS4490:1989

Samples Received 30.07.98

Client: Naylor Conservation

Unit H3 Halesfield 19 Telford, Shropshire TF7 4QT Order No.



Met Lab Ref: ME479-2 Client/Ref Description: §" Plate

Plate No.: 2 Magnification: X100 Etchant: 2% Nital Grain Size Index: III

Comments:

Sample ME479-2 etched in 2% Nital showing a microstructure consisting of large non-uniform slag inclusions in a coarse ferritic matrix typical of a poor quality wrought iron.

2 October 1998

Report Date

10 B R Whitney

Signature

Specimens will be retained for 2 months unless otherwise notified to the Laboratory

CONSULTING, INSPECTING AND TESTING ENGINEERS



Metallurgy Laboratory 40 Grosvenor Gardens London SW1W OLB Telephone 0171 565 7000 Facsimile 0171 565 7100

17499/M/5

Test Date 16-17.09.98

Samples Received

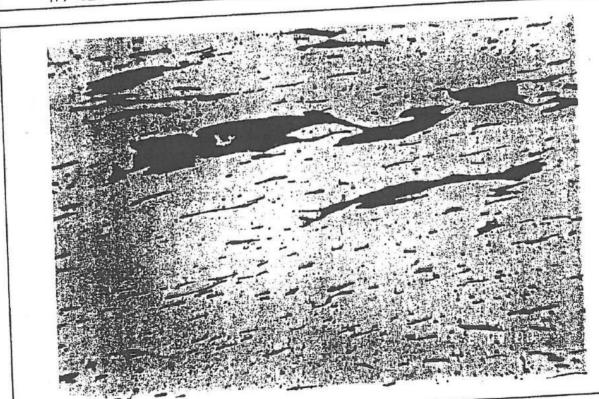
30.07.98

Order No.

METALLOGRAPHIC EXAMINATION CERTIFICATE to BS4490:1989

Client: Naylor Conservation

Unit H3 Halesfield 19 Telford, Shropshire TF7 4QT



	1.05400.1	ME480-1		Client/Ref Description:		1" Plate	
let Lab Ref:				2% Nital	Grain Size Index:	m	
late No.: 3	Magnification:	X100	Etchant:		ure consisting of	-	

Comments: Sample ME480-1 etched in 2% Nital showing a microstructure consisting of large nonuniform slag inclusions in a coarse ferritic matrix typical of a poor quality wrought iron.

2 October 1998

Report Date

Signature

BR Whitney

Specimens will be retained for 2 months unless otherwise notified to the Laboratory

CONSULTING, INSPECTING AND TESTING ENGINEERS



Metallurgy Laboratory 40 Grosvenor Gardens London SW1W OLB Telephone 0171 565 7000 Facsimile 0171 565 7100

17499/M/6

Test Date

16-17.09.98

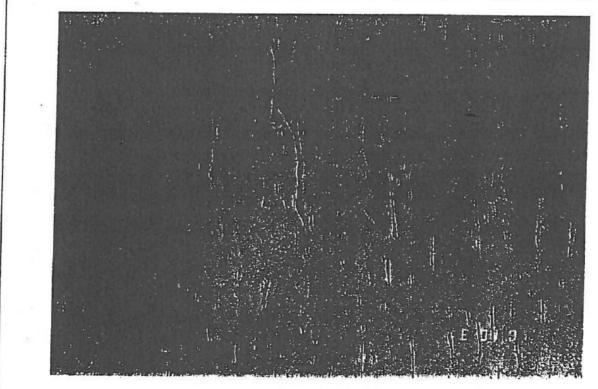
METALLOGRAPHIC EXAMINATION CERTIFICATE to BS4490:1989

Samples Received 30.07.98

Client: Naylor Conservation

Unit H3 Halesfield 19 Telford, Shropshire **TF7 40T**

Order No.



Met Lab Ref:		ME480-1	ME480-1		escription:	6" x 3" Angle	
Plate No.:	4	Magnification:	X100	Etchant:	2% Nital	Grain Size Index:	111
Comments		le ME480-1 etche m slag inclusions i					

2 October 1998

Report Date

Signature

Specimens will be retained for 2 months unless otherwise notified to the Laboratory

STATE OF THE THE STATE OF THE S

CONSULTING, INSPECTING AND TESTING ENGINEERS



Metallurgy Laboratory 40 Grosvenor Gardens London SW1W OLB Telephone 0171 565 7000 Facsimile 0171 565 7100

17499/M/7

Test Date

16-17.09.98

METALLOGRAPHIC EXAMINATION CERTIFICATE to BS4490:1989

Samples Received 30.07.98

Client: Naylor Conservation Unit H3 Halesfield 19 Telford, Shropshire TF7 4QT

Order No.

Met Lab Ref:		ME481-2		Client/Ref Description:		1/2" Pinte	
Wet Lab nei.					2% Nital	Grain Size Index:	m
Plate No.:	5	Magnification:	X100	Etchant:	2% IVILAI	Giani, Ta	

Comments:

Sample ME480-2 etched in 2% Nital showing a microstructure consisting of large nonuniform slag inclusions in a coarse ferritic matrix typical of a poor quality wrought iron.

2 October 1998

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Telephone 0171 565 7000 Facsimile 0171 565 7100 40 Grosvenor Gardens Metallurgy Laboratory London SW1W 0LB

17499/M/8

Test Date 30.9.98 Samples Received

31.7.98

Order No.

Tensile and compression testing of rivetted samples in

shear.

TF7 4QT

Telford, Shropshire

Halesfield 19

Unit H3

Naylor Conservation

Client

TEST CERTIFICATE

Test:

The riviet did not shear with the parent plate tearing away around Failure mode Maximum Load (kN) 110 Dia. of Rivets No. of Rivets N Test Mode Tensile Met Lab Ref.

The riviet did not shear with the plates seperating and pulling off the The riviet did not shear with the parent plate buckling either side of The riviet did not shear with the parent plate tearing away around

head of the corroded rivet.

one of the rivets.

94.4

N

Tensile

ME 479

ME 479

Tensile

ME 479

73.7

158

Compression

ME 479

Compression

ME 479

150

426

=

2

Compression

ME480

one of the rivets.

Failure by shearing through the single rivet.

the rivetted connection.

Failure by shearing through the two rivets.

2 October 1998

LAB FORM No. MET/101/A

Report Date

Specimens will be retained for 2 months unless otherwise notified to the Laboratory B R Whitney

The state of the s

Stormer Stormer Cont.

Signature

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Metallurgy Laboratory 40 Grosvenor Gardens London SW1W OLB Telephone 0171 565 7000 Facsimile 0171 565 7100

17499/M/9

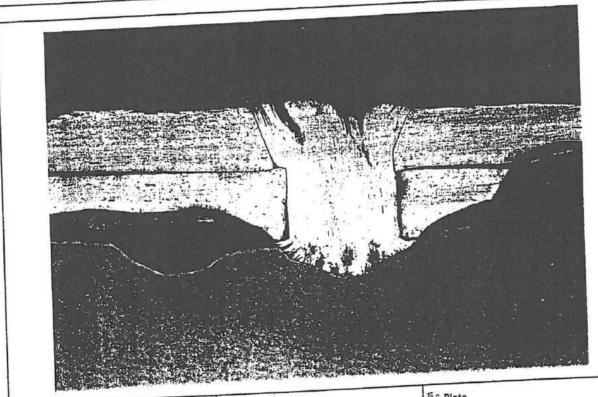
Test Date 16-17.09.98

Samples Received 30.07.98

MACROGRAPHIC EXAMINATION CERTIFICATE to BS6533:1984

Client: Naylor Conservation Unit H3 Halesfield 19 Telford, Shropshire TF7 4QT

Order No.



	205470.1	Client Ref/Description:		용" Plate	
let Lab Ref:	ME479-1			Etchant:	10% Nital
late No.:	-	Magnification:	x 1.25	Etchant.	

Comments:

Sample ME479-1 showing a typical section through the rivitted connection. This shows the large slag inclusions distributed within the plate and nickel material together with the ingress of corrosion product into the head and point of the rivet.

2 October 1998

Report Date

Signature

Specimens will be retained for 2 months unless otherwise notified to the Laboratory

CONSULTING, INSPECTING AND TESTING ENGINEERS



TESTING No. 0957 Metallurgy Laboratory 40 Grosvenor Gardens London SW1W 0LB Telephone 0171 565 7000 Facsimile 0171 565 7100

17499/M/10

Test Date

16-17.09.98

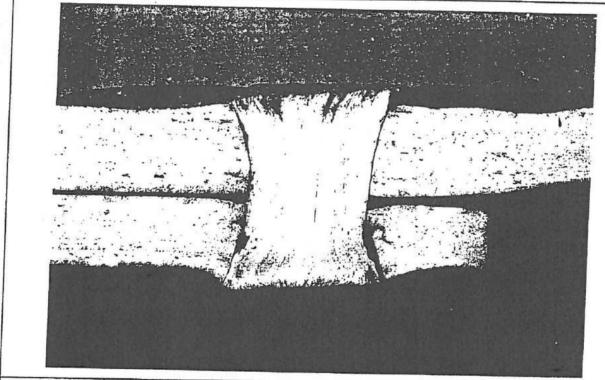
MACROGRAPHIC EXAMINATION CERTIFICATE to BS6533:1984

Samples Received

30.07.98

Client: Naylor Conservation

Unit H3 Halesfield 19 Telford, Shropshire TF7 4QT Order No.



Met Lab Ref: ME480-1 Client Ref/Description: 1" Plate

Plate No.: 7 Magnification: x 1.25 Etchant: 10% Nital

Comments:

Sample ME480-1 showing a typical section through the rivitted connection. This shows the large slag inclusions distributed within the plate and nickel material together with the ingress of corrosion product into the head and point of the rivet.

2 October 1998

Report Date

MB R Whitney

Signature

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CONSULTING, INSPECTING AND TESTING ENGINEERS



No. 0957

Metallurgy Laboratory 40 Grosvenor Gardens London SW1W OLB Telephone 0171 565 7000 Facsimile 0171 565 7100

17499/M/11

Test Date

16-17.09.98

Samples Received 30.07.98

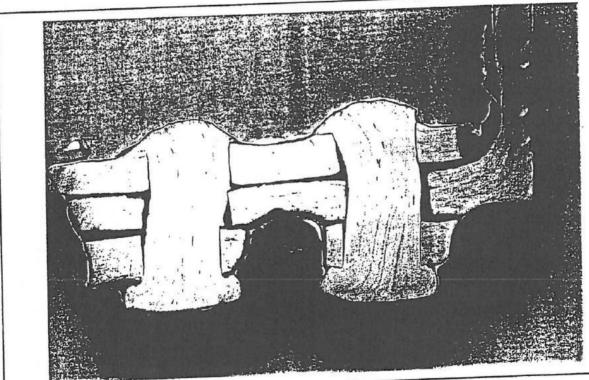
MACROGRAPHIC EXAMINATION CERTIFICATE to BS6533:1984

Client: Naylor Conservation

Unit H3 Halesfield 19 Telford, Shropshire

TF7 4QT

Order No.



Met Lab Ref: ME481-1		Client Ref/Descrip	tion:	6" x 3" Angle		
Wet Lab her:				10% Nital		
Plate No.:	R	Magnification:	× 1	Etchant:	10 /0 /11	

Comments:

Sample ME481-1 showing a typical section through the rivitted connection. This shows the large slag inclusions distributed within the plate and nickel material together with the ingress of corrosion product into the head and point of the rivet.

2 October 1998

Report Date

Signature

A) BR Whitney

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CONSULTING, INSPECTING AND TESTING ENGINEERS



Metallurgy Laboratory 40 Grosvenor Gardens London SW1W 0LB Telephone 0171 565 7000 Facsimile 071 565 7100

17499/M/12

Test Date 14.9.98

Samples Received 31.7.98

TEST CERTIFICATE

Client: Naylor Conservation

Unit H3 Halesfield 19 Telford, Shropshire TF7 4QT Order No.

CHEMICAL ANALYSIS
DETERMINATION OF CHLORIDE CONTENT
TO BS 1881:Part 124:1988

Met Lab Ref	Client Ref / Description	% Chloride by weight
ME 594	Corrosion Sample No. 2	0.04
ME 595	Corrosion Sample No. 3	0.03
ME596	Corrosion Sample No. 4	0.01
ME597	Corrosion Sample No. 5	0.01

2 October 1998 Report Date 1 B R Whitney Signature

Specimens will be retained for 2 months unless otherwise notified to the Laboratory

STANCE SCHOOL SUITALIS TOUTHER BOUND HAVING FEATURE OF COURSE OF COMPANY OF THE CONTRACT OF THE CONTRACT OF THE

CONSULTING, INSPECTING AND TESTING ENGINEERS

Metallurgy Laboratory 40 Grosvenor Gardens London SW1W OLB Telephone 0171 565 7000 Facsimile 071 565 7100

17499/M/13

Test Date 31.7.98

Samples Received N/A

TEST CERTIFICATE

Client: Naylor Conservation

Unit H3 Halesfield 19 Telford, Shropshire TF7 4QT

Order No.

EXAMINATION OF TIMBER TIMBER PROPS Results: Comments Approximate Load in Prop (kN) Prop Location / Number Further loading was aborted due to local Load just released at 20 kN distortion of the hull 2. Port Side Damaged prop removed Initial load released at 11kN, 4, Port Side Load off completely at 15 kN. Further loading was aborted due to local Load in prop greater than 25 kN distortion of the hull 5, Port Side Load released at 10 kN 2, Starboard Side Initial load released at 25 kN 4, Starboard Side Further loading was aborted due to local Load in prop greater than 30 kN distortion of the hull 5, Starboard Side Buckling in the prop would indicate high loads Not tested in this area greater than 30 kN. 7, Starboard Side Buckling in the prop would indicate high loads Not tested in this area greater than 30 kN. 8, Starboard Side Buckling in the prop would indicate high loads Not tested in this area greater than 30 kN. 9, Starboard Side Buckling in the prop would indicate high loads Not tested in this area greater than 30 kN. 11, Starboard Side

Comments: Props numbered from bow to stern of the ship. Six timber props, three from each side were examined to determine the load in each prop. A secondary support prop incorporating a hydraulic ram and calibrated load cell was positioned adjacent to each of the props. Jacking of the secondary prop was continued until the load was released in the original prop or the maximum capacity of the jacking system was achieved.

2 October 1998

Report Date

BR Whitney

Signature

Specimens will be retained for 2 months unless otherwise notified to the Laboratory

CONSULTING, INSPECTING AND TESTING ENGINEERS Metallurgy Laboratory 40 Grosvenor Gardens London SW1W 0LB Telephone 0171 565 7000 Facsimile 071 565 7100

17499/M/14a

Test Date 31.7.98

Samples Received N/A

TEST CERTIFICATE

Client: Naylor Conservation

Unit H3 Halesfield 19 Telford, Shropshire TF7 4QT Order No.

INSPECTION OF COFFER DAM

OUTSIDE FACE OF DAM THICKNESS READINGS FOR EACH PANEL (mm)

TOP

					1			1
	7.5	8.0	7.2	7.7	7.9	7.8	8.0	7.9
	7.5	7.8	7.4	6.8	7.3	7.4	7.9	8.0
Floor	7.0	7.1	8.7	8.7	9.0	9.5	8.5	8.8
-	6.7	8.6	8.8	8.7	7.9	8.8	8.8	8.9
	N/A	8.6	8.8	8.7	7.8	8.5	8.7	N/A

воттом

Comments:

The plan of the coffer dam as shown above represents the panels outlined by the framing on the inside of the structure. The plan of the face of the coffer dam is shown as viewed from inside the dock.

Readings on each panel are based on three readings taken using a calibrated ultrasonic thickness probe.

The base of the coffer dam was found to be filled with mass concrete.

4 October 1998

Report Date

___ Signature

Specimens will be retained for 2 months unless otherwise notified to the Laboratory

BR Whitney

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CONSULTING, INSPECTING AND TESTING ENGINEERS

Metallurgy Laboratory 40 Grosvenor Gardens London SW1W OLB Telephone 0171 565 7000 Facsimile 071 565 7100

17499/M/14b

Test Date 31.7.98

Samples Received N/A

TEST CERTIFICATE

Client: Naylor Conservation

Unit H3 Halesfield 19 Telford, Shropshire TF7 4QT

Order No.

INSPECTION OF COFFER DAM

INSIDE FACE OF DAM THICKNESS READINGS FOR EACH PANEL (mm)

TOP

	1000						
7.1	7.7	7.5	7.8	7.6	7.7	8.0	7.9
7.4	7.5	7.4	7.1	7.2	7.3	7.6	7.7
8.8	8.9	8.8	8.8	8.6	8.4	8.9	8.8
8.6	8.8	8.8	8.7	8.5	8.7	8.8	8.7
N/A	7.5	8.6	7.9	8.7	8.7	8.7	N/A

BOTTOM

Comments:

Floor

The plan of the coffer dam as shown above represents the panels outlined by the framing on the inside of the structure. The plan of the face of the coffer dam is shown as viewed from inside the dock.

Readings on each panel are based on three readings taken using a calibrated ultrasonic thickness probe.

The base of the coffer dam was found to be filled with mass concrete.

4 October 1998

Report Date

Signature

Specimens will be retained for 2 months unless otherwise notified to the Laboratory

APPENDIX A

PLATE NUMBERS 9 to 17

Q. 1

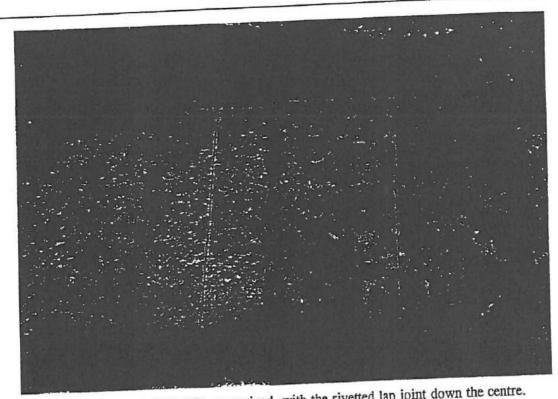


Plate No.9 Showing sample ME 479, as received, with the rivetted lap joint down the centre.

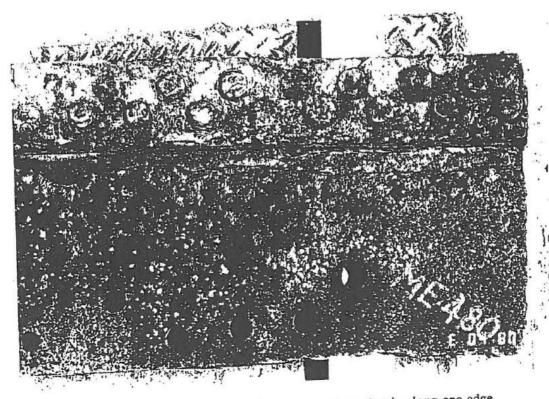


Plate No.10 Showing sample ME 480, as received, with the rivetted strip along one edge.

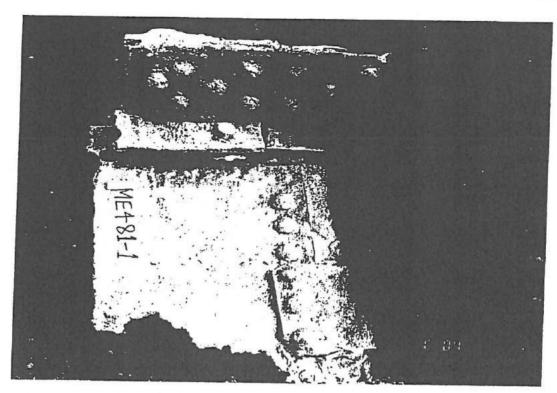


Plate No.11 Showing sample ME 481 a compound rivetted section with plate and angle sections, as received at the Laboratory.

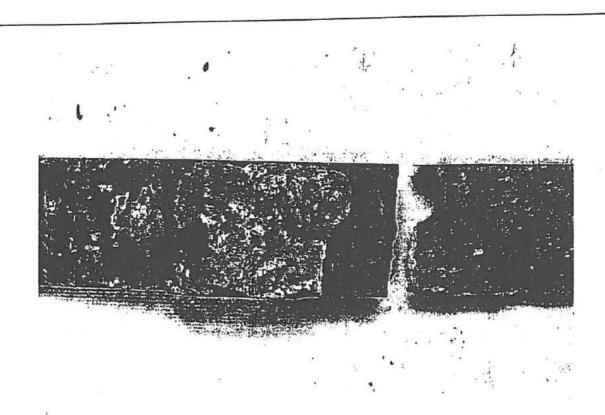


Plate No.12 Showing a tensile test specimen taken across the rivetted joint after testing. This shows the sample failing by tearing of the parent plate around the rivets rather than due to shearing of the rivets.

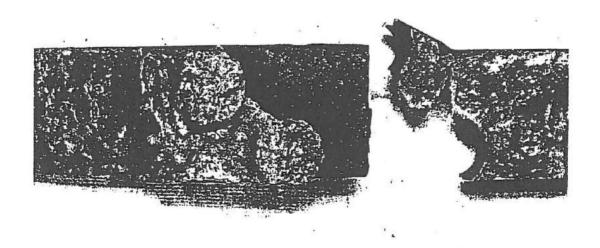


Plate No.13 Showing a tensile test specimen taken across the rivetted joint after testing. This shows the sample failing by tearing of the parent plate around the rivets rather than due to shearing of the rivets.

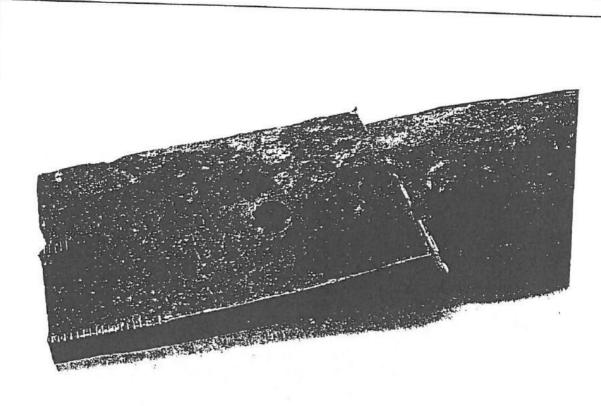


Plate No.14 Showing a shear test on a rivetted sample carried out in tension. This sample failed by the plate pulling over the badly corroded head of the rivet.

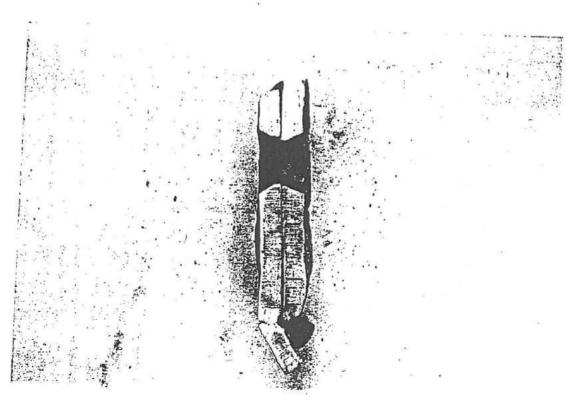


Plate No.15 Showing a shear test sample, in compression, where failure has occurred due to fracture of the parent material outside of the rivetted joint due to the large loss of section in this area.

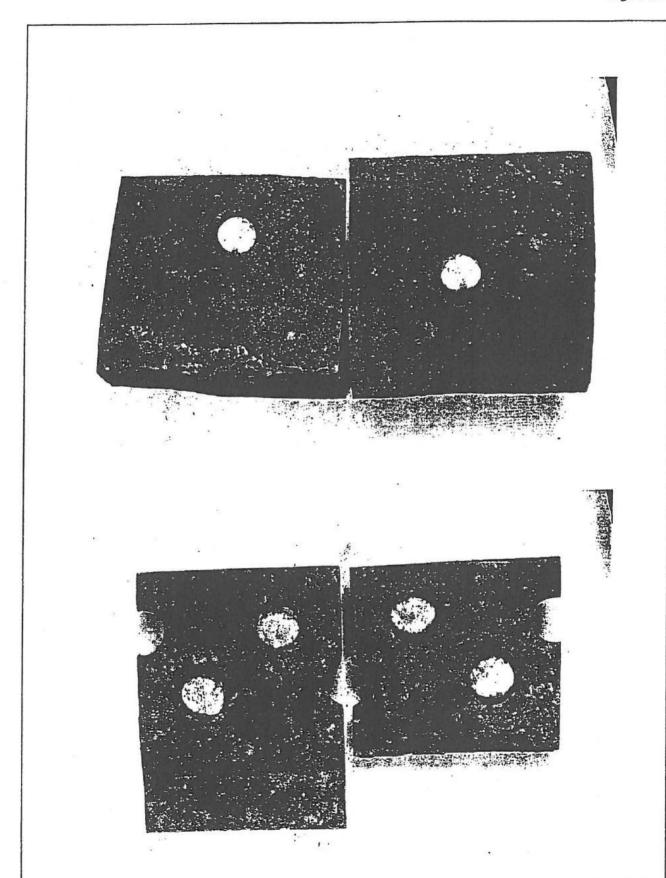


Plate Nos.16 and 17

Showing the shear mode failure of two of the samples tested in compression. Both samples contained 1" rivets which failed with typical fracture faces and distortion in the holes in the plate.

APPENDIX B

PLATE NUMBERS 18 to 20

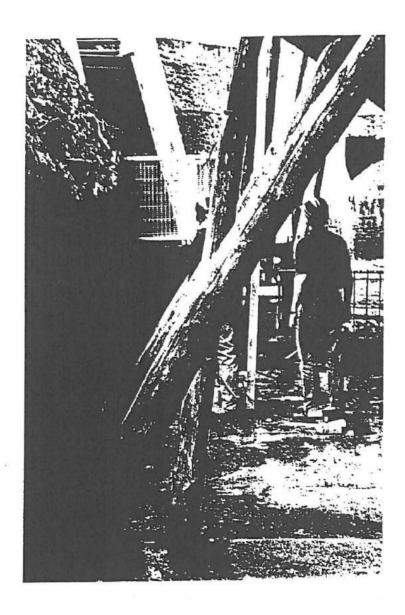


Plate No.18 Showing a view looking forward on the starboard side of the ship. This shows the distortion in the angled props where they are locked in against the side wall of the dock.

: 3



Plate No.19 Showing a view looking aft on the starboard side of the ship. This shows the distortion in the angled props where they are locked in against the side wall of the dock.

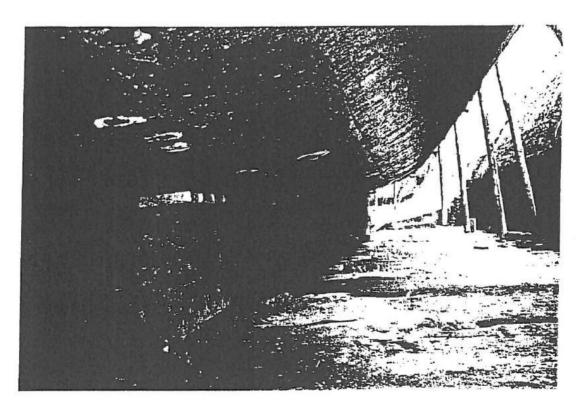


Plate No. 20 Showing a view looking forward on the starboard side of the ship. This shows the local distortion in the bilge keel where it passes over the third prop visible. This position coincides with the tear in the hull plates on this side of the ship.

Appendix F

Temporary Dam Proposal Mowlem Civil Engineering, September 1998.

SS Great Britain Project

Great Western Dry Dock

Temporary Dam Proposal

Prepared for

ura Conservation Ltd
Unit H3
Halksfield 19
Telford
Shropshire TF7 4QT

Central Engineering Services
Mowlem Civil Engineering,
Foundation House,
Eastern Road,
Bracknell,
Berkshire. RG12 2UZ
Tel: 01344 426826 fax: 01344 862027

September 1998

Brief

An outline scheme is required for a temporary dam across the entrance to the Great Western Dry dock to enable the full examination of the existing dry dock caisson. The Dry Dock is located in the Bristol City Docks.

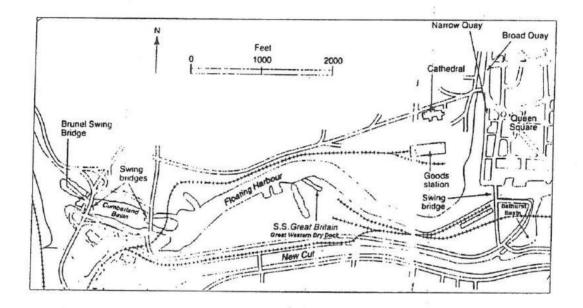


Figure 1. Dry Dock location

Dry Dock

The Dry dock was built around 1840 specifically for the construction of the SS Great Britain. The original Dock layout is shown in figure 2.

Ground Conditions

A drawing of the dry dock and the information contained in the archaeological appraisal indicate that the entrance to the dry dock has been silted to a depth of about one and a half metres above the dock sill level. This silting reduces closer to the main channel. It is assumed that the silt and debris across the dock entrance will be dredged clear before the temporary dam is installed.

Historical accounts of the construction of the floating harbour basins (Cumberland and Bathurst) and the New Cut indicate that the underlying ground consists of soft clays and silts above rock. The only definitive information we have about the underlying rock level is from the Cumberland basin where the rock is about 17m below ground level. The same source also confirms the presence of soft clays and silts.

The docks are non tidal with the water level controlled by locks and sluices therefore no large variations in water level are expected. Design has been based on the normal dock and the HWST levels given in the reference documents.

Dock levels

References levels for the dry dock and approach channel are taken from figure 2.

Level (feet)	Level (metres)
	8.34
	9.144
31.58	9.625
35.00	10.688
	4.831
15.05	4.544
	h = 9.144 - 4.544 = 4.6 m
	Level (feet) 27.36 30.00 31.58 35.00 15.85